52 W low-cost two-stage LED driver based on ICL5102

A PFC + open-loop LCC design with tight LED current spread

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About this document

Scope and purpose

ICL5102 is an integrated combo controller IC designed to drive and control the boost PFC + resonant half-bridge (HB) topology (LLC/LCC) in combination. The superior performance of its THD optimizer in the PFC part makes it very suitable for LED lighting applications. Infineon's proprietary coreless transformer-based high-side MOSFET driver enables a robust HB drive at high operating frequency.

This work demonstrates a highly efficiently low-cost non-dimmable PFC + LCC LED driver based on **ICL5102**. Thanks to the integrated, robust and efficient HB MOSFET driver, the LCC stage is designed at high operating frequency (up to 250 kHz) to realize an integrated resonant transformer at lower cost. In this non-dimmable design, open-loop control is implemented for further cost reduction. The LCC resonant tank is designed in a particular manner for a tight LED current tolerance (±10 percent), over a wide temperature range and with most IC and component tolerance taken into account. This is of great importance in the open-loop product design.

This report documents the experimental test results of this 52 W open-loop LCC demonstration board and LED current spread analysis.

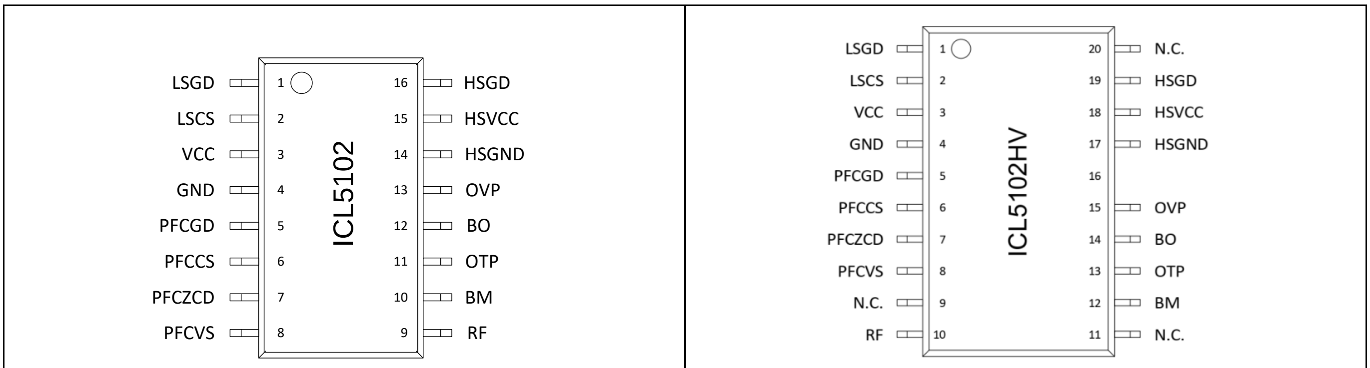
Intended audience

This document is intended for technical experts who intend to use this **ICL5102** demonstration board, either for their own applications and **ICL5102** function tests, or as a reference for a new **ICL5102**-based product development.

Table of contents

1 IC introduction

ICL5102 is an integrated combo IC which is designed to drive and control the boost PFC + resonant HB topology (LLC/LCC) in combination. Its high-voltage version, **ICL5102HV**, can handle 980 V (maximum value) on the half-bridge part, which is the highest voltage rating on the market so far. The pin maps of **ICL5102** and **ICL5102HV** are given in **Figure 1**. Thanks to Infineon’s proprietary coreless transformer technology, **ICL5102HV**’s high-side MOSFET driver is very robust against dV/dt and negative voltage peak in the middle point of the half-bridge, and generates low loss at high operating frequency.



(a) **ICL5102** – PG-DSO-16 package | **(b) ICL5102HV** - PG-DSO-19-1 package

Figure 1 Pin maps of (a) ICL5102 and (b) ICL5102HV

The other key features of **ICL5102** are summarized as follows:

Key features:

- Integrated two-stage combo controller allowing for reduced number of external components, optimized bill of materials (BOM) and form factor.
- PFC controller with critical conduction mode (CrCM) and discontinuous conduction mode (DCM).
- Resonant HB controller with fixed or variable switching frequency control.
- Maximum 500 kHz HB switching frequency and soft-start frequency up to 1.3 MHz.
- Resonant HB burst mode (BM) ensures power limitation and low standby power of less than 300 mW.
- Supports universal AC input voltage.
- Supports excellent system efficiency.
- THD optimization ensuring low harmonic distortion down to 30 percent nominal load.

Protection mechanisms:

- Input brown-out protection.
- PFC bus overvoltage protection (OVP).
- PFC over-current protection (OCP).
- Output OVP, OCP/short-circuit protection.
- Output overpower/overload protection (OPP).
- HB capacitive mode protection.
- Overtemperature protection (OTP).

2 Board description

This 52 W demonstration board is developed for non-dimmable applications with 198 V AC ~ 264 V AC input voltage and 52 V ~ 20 V LED voltage range. The output current is selectable with a two-channel switch. The system architecture of this design is shown in **Figure 2**.

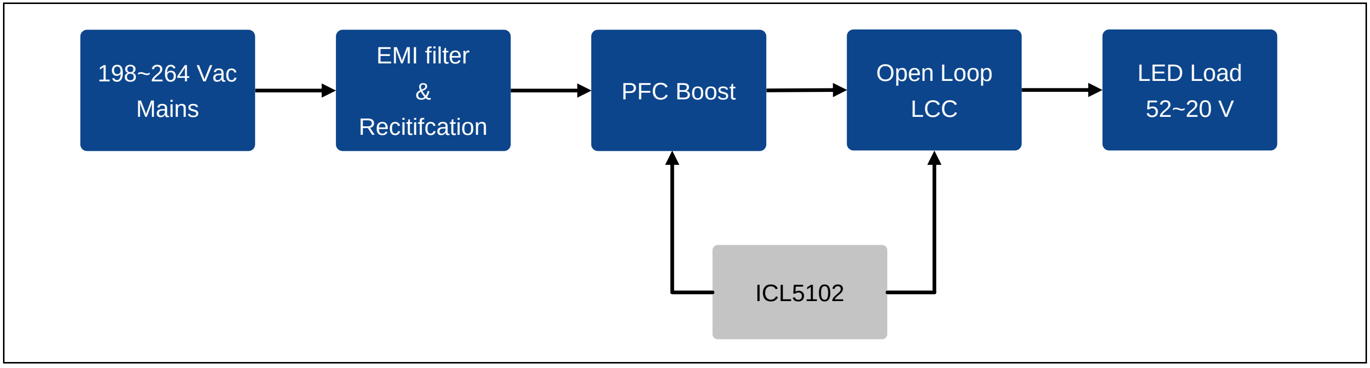


Figure 2 System architecture

Key features of this non-dimmable demonstration board are:

- Low system cost realized with open-loop LCC design and resonant inductor integrated within the LCC transformer.
- LED current tolerance is tightly controlled across a wide temperature range and standard component spread.
- High system efficiency from a dedicated LCC resonant tank design principle for in this non-dimmable application.
- High LCC operating frequency.

2.1 Electrical specifications

Table 1 lists the key electrical specifications of this demonstration board.

Table 1 Key electrical specifications

Parameters	Symbol	Min.	Typ.	Max.	Unit	Remarks
AC input voltage	$V_{in(ac)}$	198	220230	256	V_{RMS}	
Input frequency	f_{in}	47		63	Hz	
Inrush current	$I_{in(pk)}$			35	A_{pk}	
Total harmonic distortion	THD			10 percent	–	Full load range and input voltage range
Efficiency	η		92.5 percent		–	At the maximum load
Targeted LED voltage	V_{LED}	20		52	V DC	
LED current setting 1	$I_{LED.s1}$		1000		mA	V_{LED} = 20 ~ 52 V -20°C ~ 100°C[1]
Current spread at setting 1	$\Delta I_{LED.S1}$		± 10 percent			
LED current setting 2	$I_{LED.s2}$		0.88		mA	
Current spread at setting 2	$\Delta I_{LED.S2}$		± 10 percent			
LED current setting 3	$I_{LED.s3}$		0.78		mA	V_{LED} = 26 ~ 52 V -40°C ~ 125°C[2]
Current spread at setting 3	$\Delta I_{LED.S3}$		± 10 percent			
LCC frequency	f_{LCC}	160		270	kHz	
PFC frequency	f_{PFC}	15			kHz	
Brown-out voltage	V_{BO}		180		V AC	
Brown-in voltage			195		V AC	
EMI	EN 55015					
Harmonics	EN 61000-3-2 class C					

[1] IC junction temperature
[2] IC junction temperature

2.2 Schematic and layout

The following figures illustrate the schematic and layout of the board, respectively. On the top side of this single-sided PCB only through-hole components are placed. The copper thickness is 70 µm (2 oz).

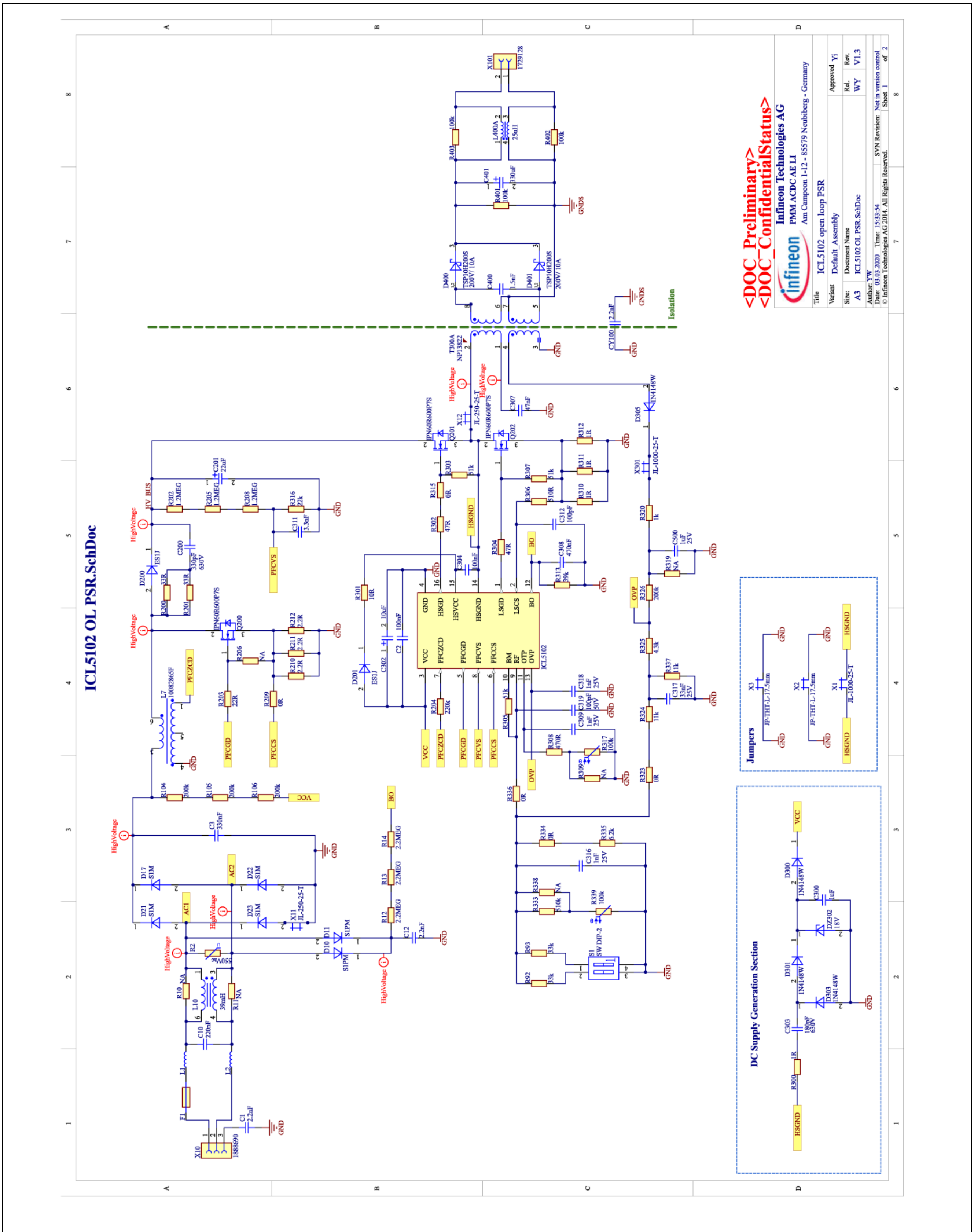


Figure 3 **Schematic**

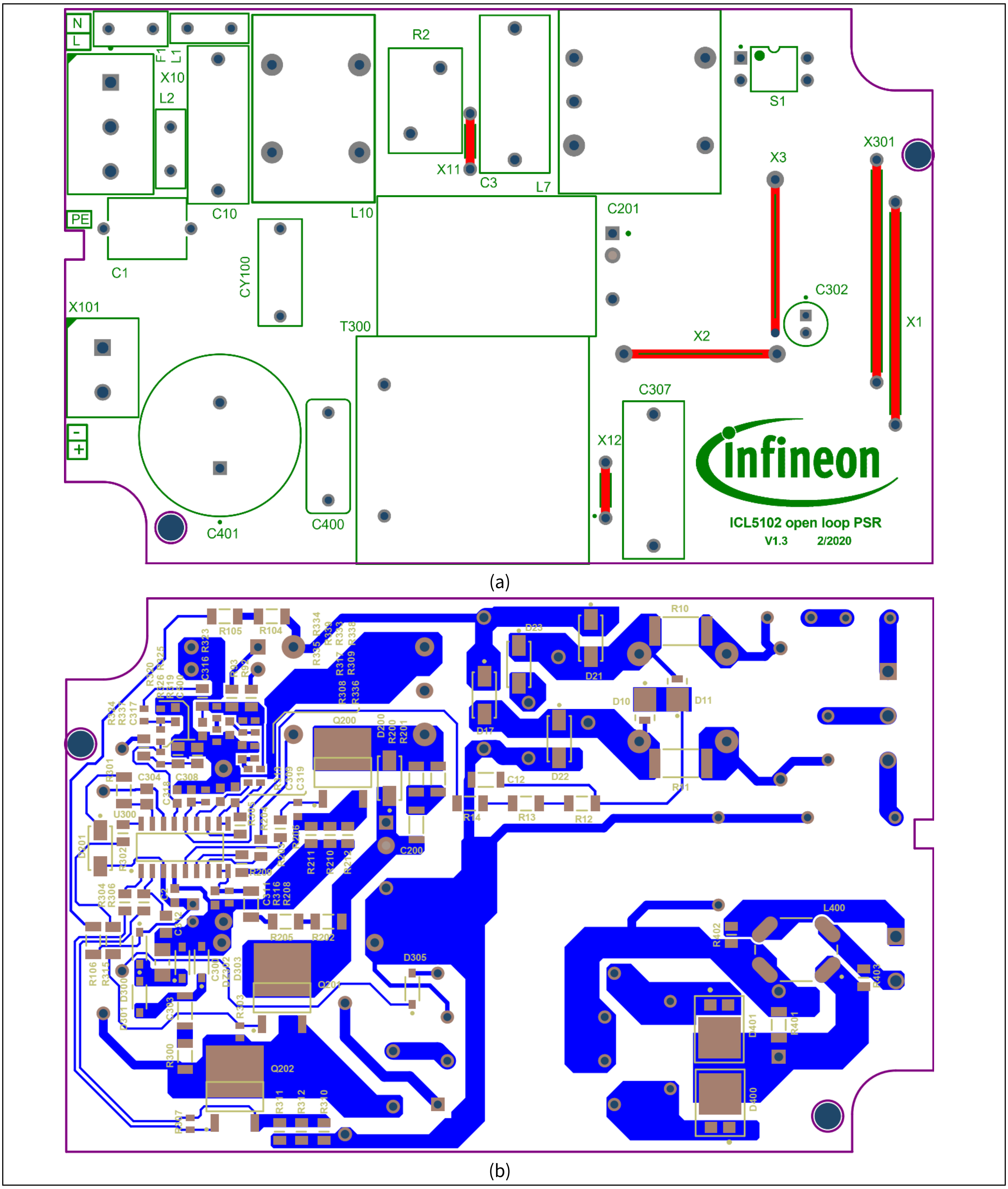


Figure 4 **Board layout – (a) top side and (b) bottom side**

2.3 Board setup

Figure 5 Board setup

3 Electrical performance

This reference board is designed to be a non-dimmable LED driver, with three selectable output current settings that can be configured by a mechanical switch. One important design target is to guarantee the LED current spread is less than or equal to 10 percent over a wide temperature range and a wide LED voltage range within the given component spread. The specified operating area is given in **Figure 6**.

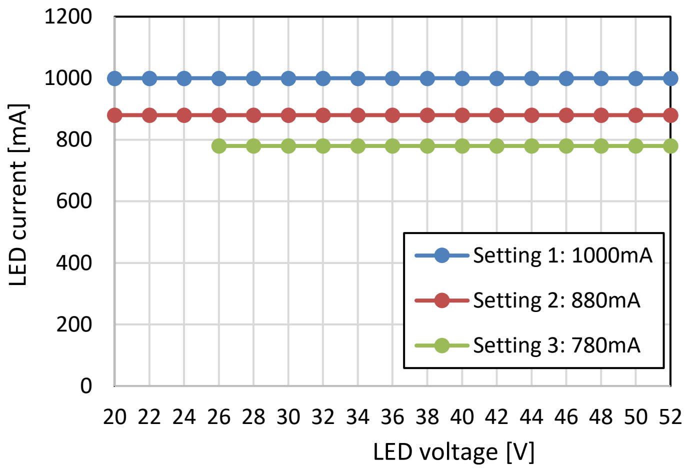


Figure 6 Driver operating windows

The electrical performance of the system, the PFC and and the LCC are presented below. Additonally, the LED current spread analysis is also conducted.

3.1 System performance

The system performance in steady-state at three current settings is presented below. They cover the system efficiency at different conditions (Figures 7 and 8), power factor and THD (Figures 9 and 10) and harmonics at two current settings (Figures 11 and 12). The efficiency at maximum load and 230 V AC reaches 92.5 percent.

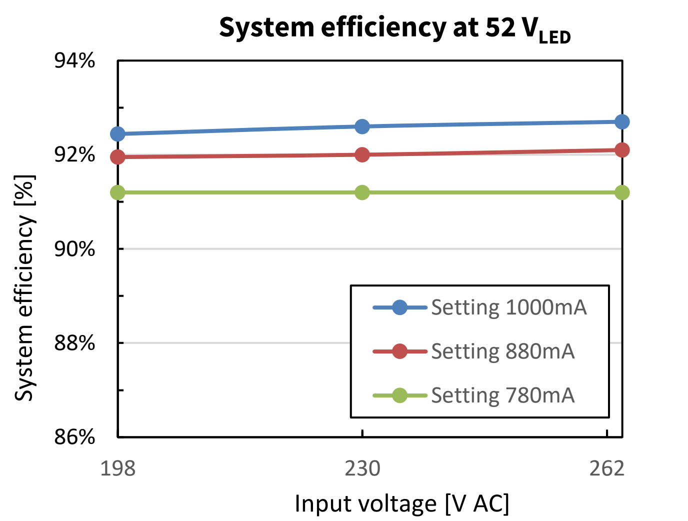


Figure 7 System efficiency at various input voltages and 52 V_{LED}

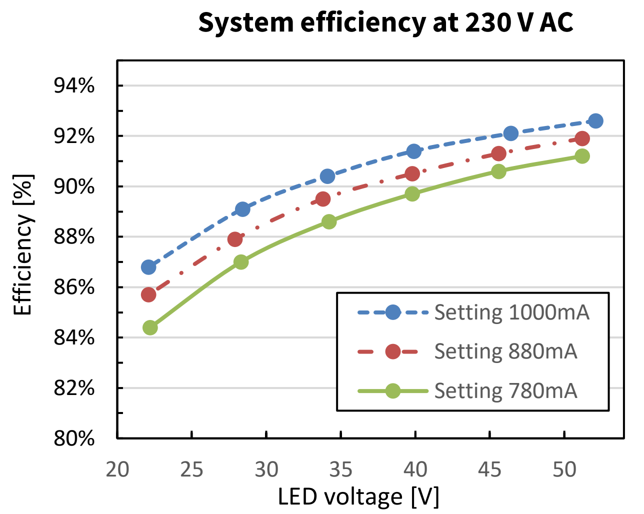


Figure 8 System efficiency at 230 V AC and various V_{LED}

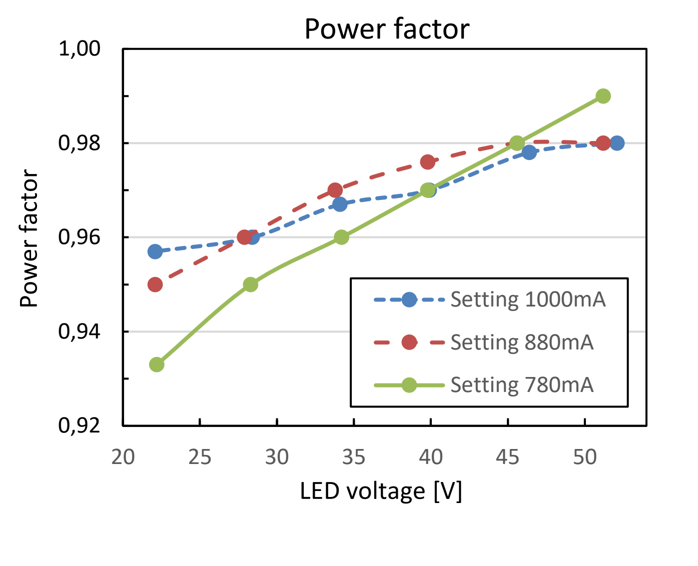


Figure 9 **Power factor**

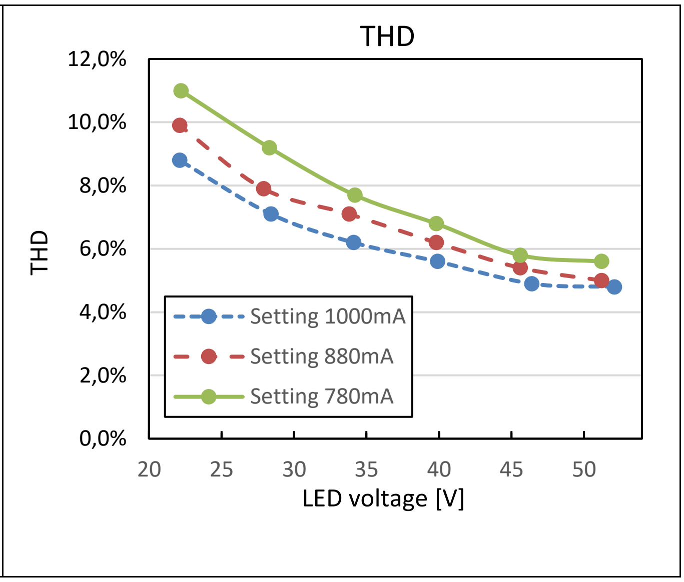


Figure 10 **Total harmonic distortion**

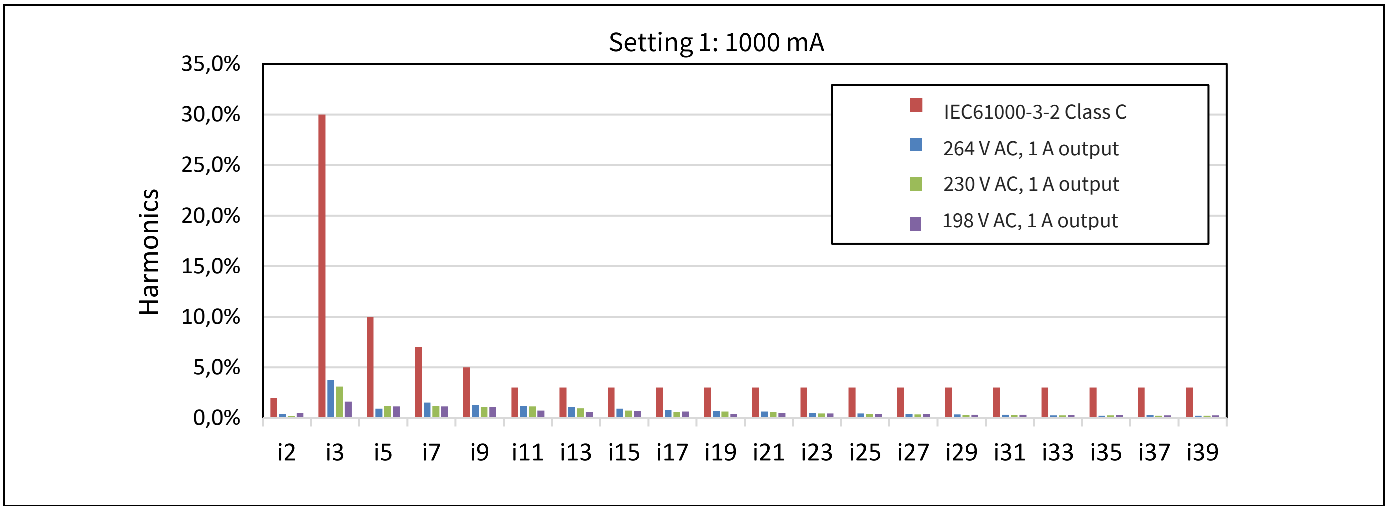


Figure 11 **Harmonics measurement at 1000 mA setting**

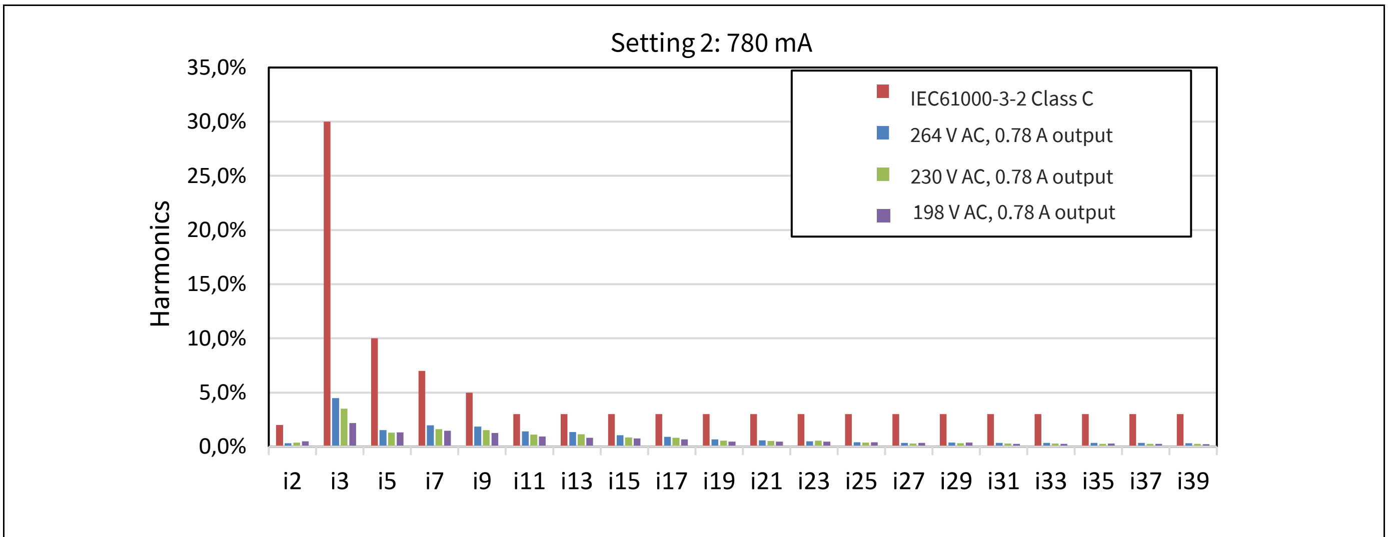


Figure 12 **Harmonics measurement at 780 mA setting**

The measured LED current at various LED voltages at three current settings is plotted in **Figure 13**. These measurements are conducted at a room temperature of 23°C.

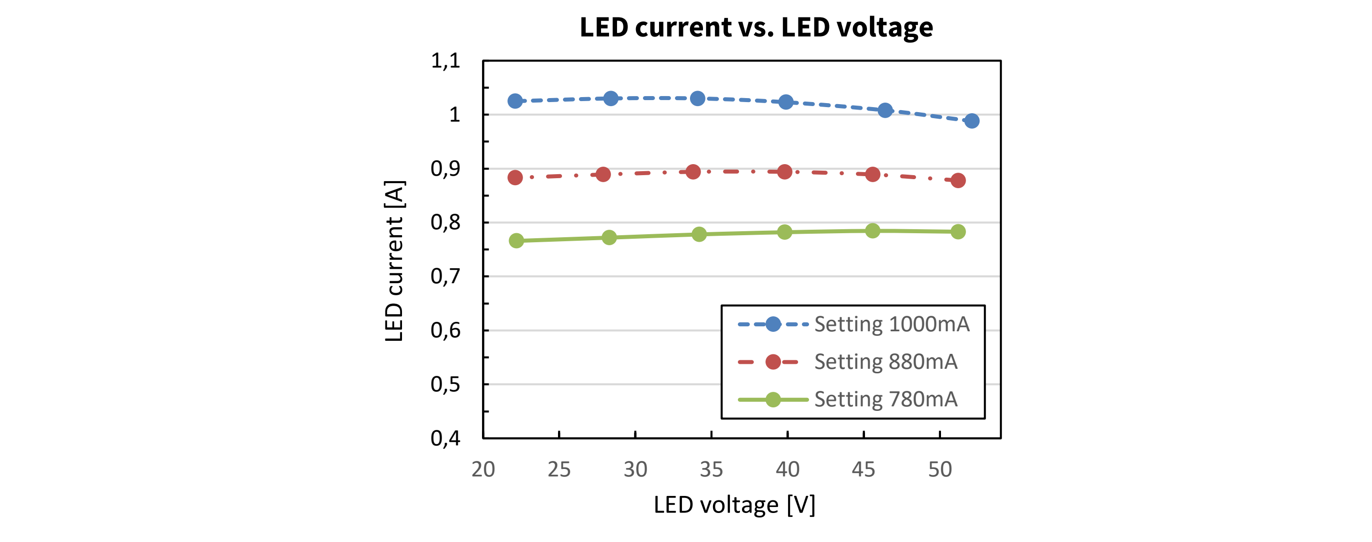
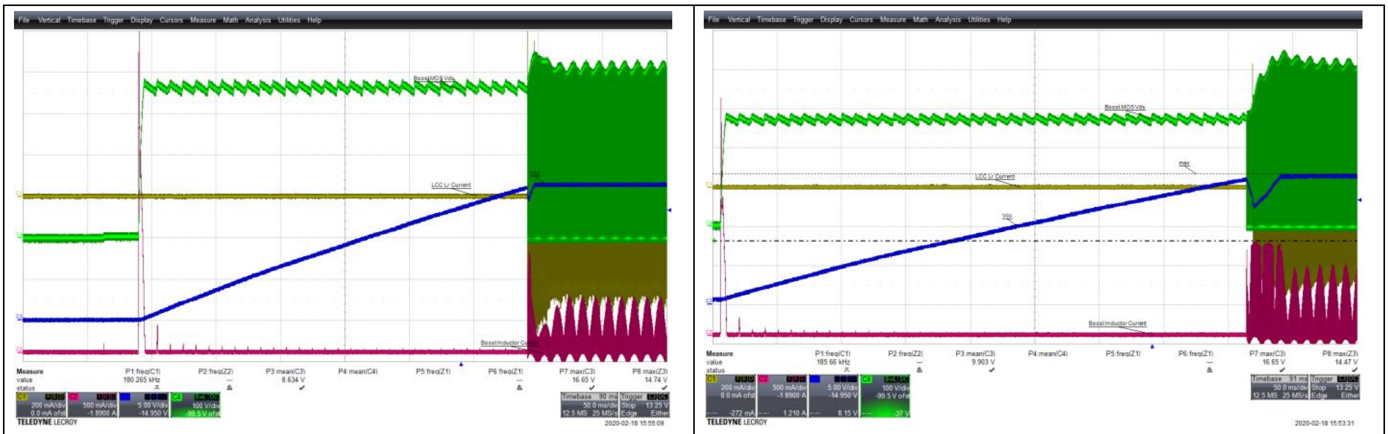


Figure 13 LED current at various LED voltage and current settings

3.2 Start-up behavior

This part presents the start-up behavior of the driver at various input voltages and loads.

The V_{CC} pull-up resistors and V_{CC} capacitor are selected such that the start-up time in the worst case is less than 500 ms (see **Figure 14**).



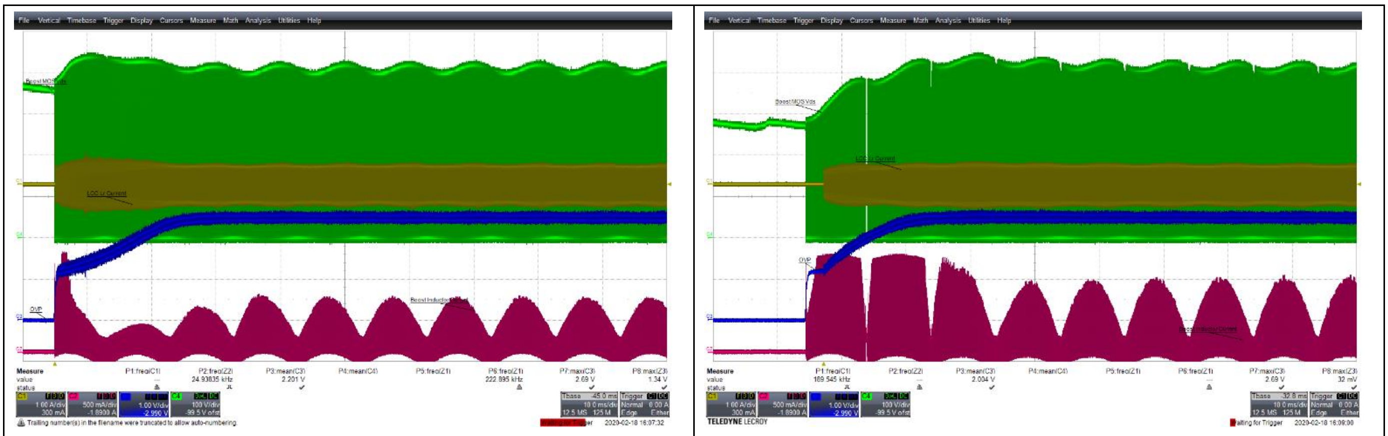
(a) 264 V AC – **315 ms** start-up time

(b) 198 V AC – **420 ms** start-up time (worst case)

CH1: Resonant inductor current in LCC, CH2: Boost inductor current, CH3: V_{CC} pin voltage, CH4: HSGND pin voltage

Figure 14 Start-up time at (a) 264 V AC and (b) 198 V AC with maximum load

The PFC start-up waveforms are given in **Figure 15**. At low mains voltage, the boost inductor current is designed to be clamped to avoid inductor saturation.



(a) 264 V AC (b) 198 V AC

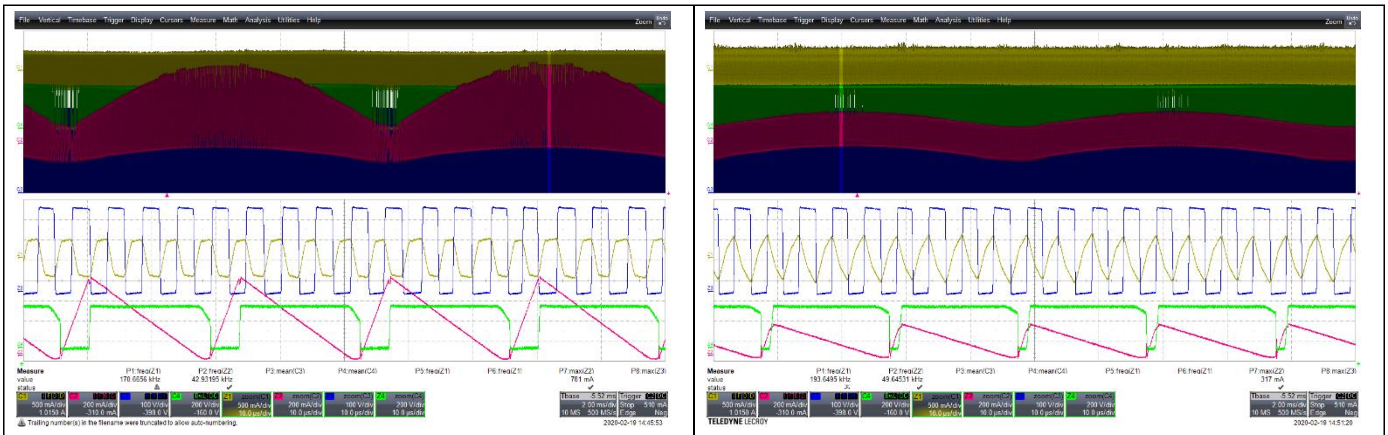
CH1: Resonant inductor current in LCC, CH2: Boost inductor current, CH3: OVP pin voltage, CH4: HSGND pin voltage

Figure 15 PFC start-up behavior at (a) 264 V AC and (b) 198 V AC

3.3 Steady-state

The key waveforms of the PFC and LCC at various input voltages and LED voltages in three current settings are measured and given below in from **Figure 16** to **Figure 19**.

At 264 V AC and 1000 mA current setting, the PFC operates in CrCM across the full LED voltage range. The average operating frequency of LCC is around 190 kHz.

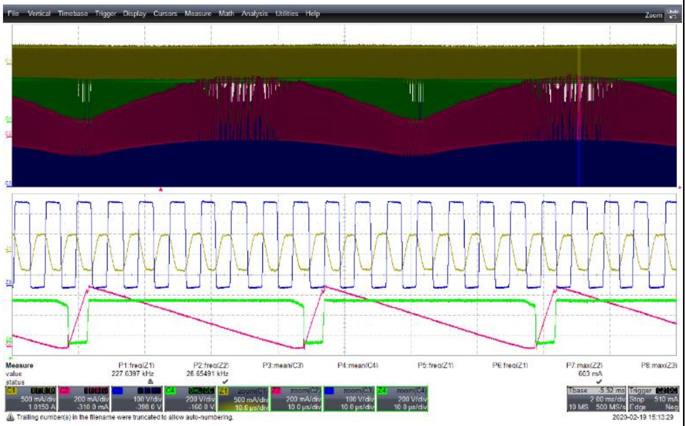


(a) **52 V**, 1000 mA (b) **20 V**, 1000 mA

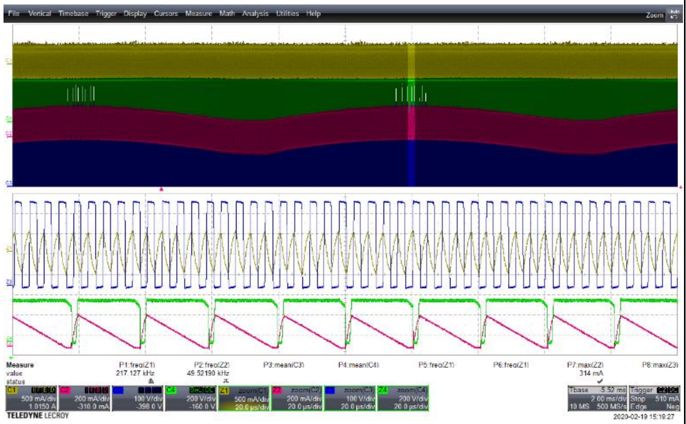
CH1: Resonant inductor current in LCC, CH2: Boost inductor current, CH3: HSGND voltage, CH4: Boost MOSFET V_{DS}

Figure 16 Steady-state waveform at 264 V AC with 1000 mA LED current

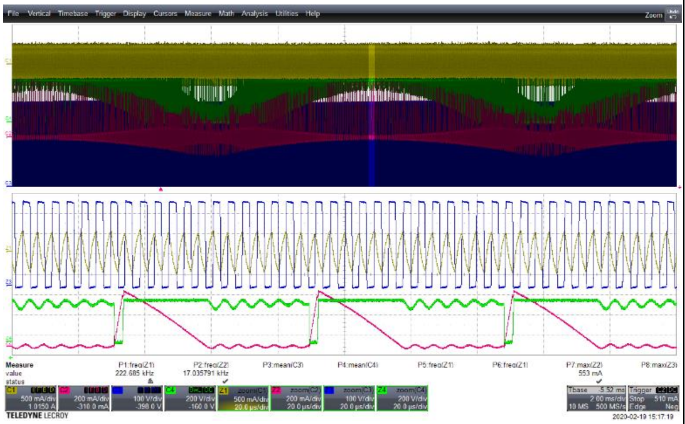
At 264 V AC and 880 mA current setting, the PFC operates in CrCM across most of the LED voltage range. At 20 V LED, the PFC operates in DCM (see **Figure 17c**) with the minimum operating frequency 17 kHz.



(a) LED load: **52 V**, 880 mA



(b) LED load: **26 V**, 880 mA

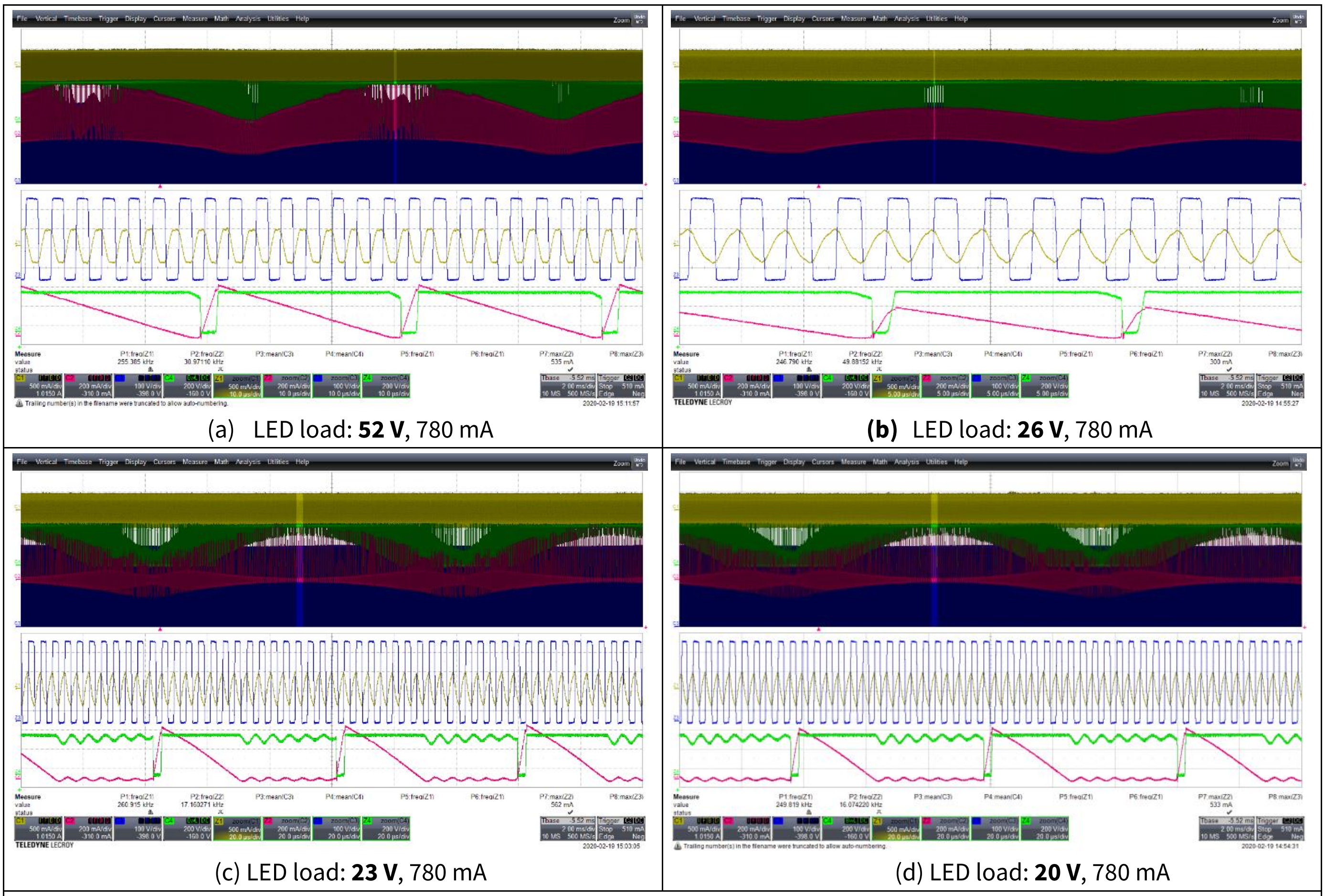


(c) LED load: **20 V**, 880 mA

CH1: Resonant inductor current in LCC
CH2: Boost inductor current
CH3: HSGND voltage
CH4: Boost MOSFET V_{DS}

Figure 17 Steady-state waveform at 264 V AC with 880 mA LED current

At 264 V AC and 780 mA current setting, the PFC operates in CrCM across most of the LED voltage range. At 20 V and 23 V LED, the PFC operates in DCM (see **Figure 18c** and **Figure 18d**) with the minimum operating frequency of 16 kHz at 20 V_{LED}.

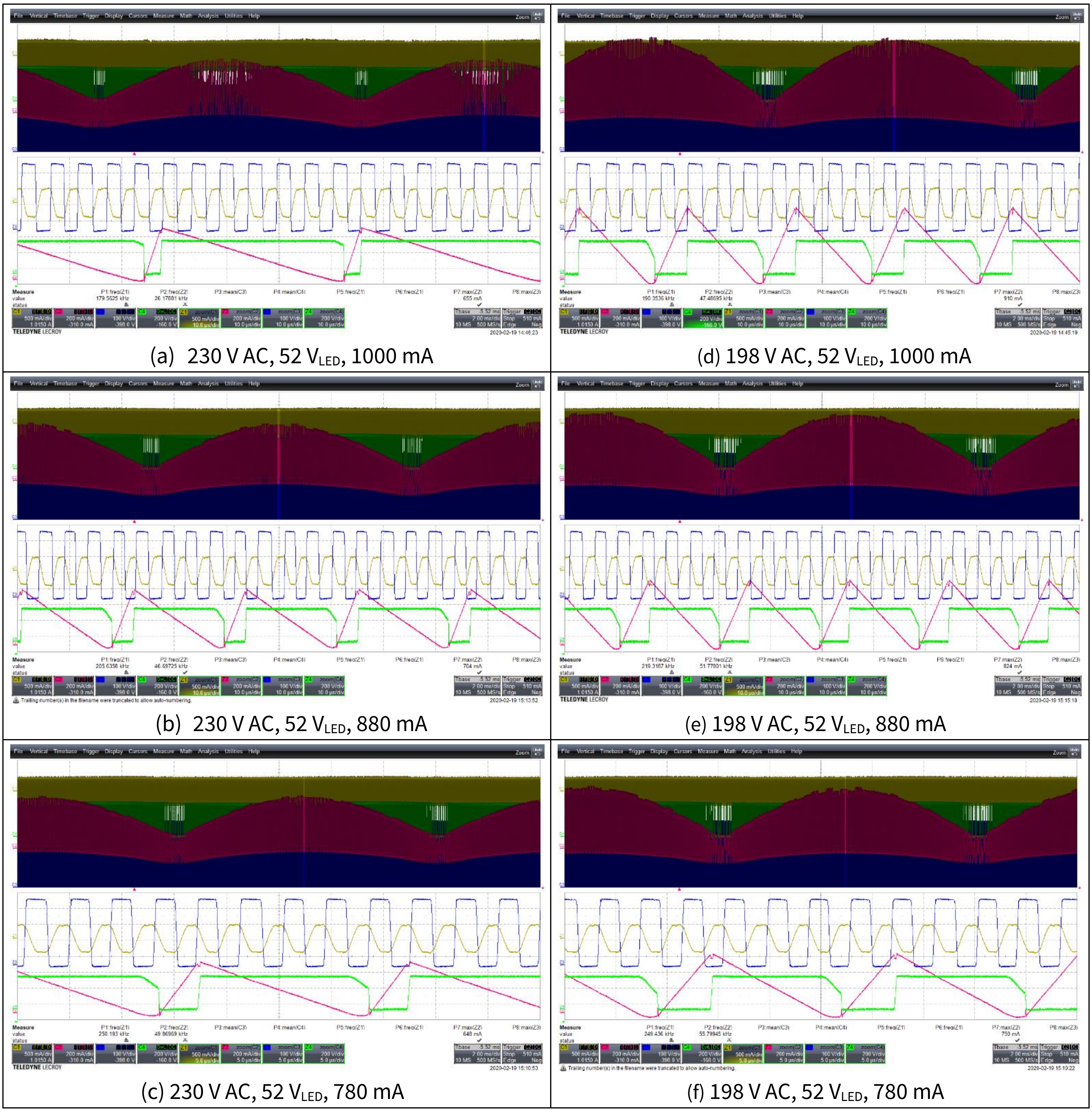


(a) LED load: **52 V**, 780 mA
(b) LED load: **26 V**, 780 mA
(c) LED load: **23 V**, 780 mA
(d) LED load: **20 V**, 780 mA

CH1: Resonant inductor current in LCC, CH2: Boost inductor current, CH3: HSGND voltage, CH4: Boost MOSFET V_{DS}

Figure 18 Steady-state waveform at 264 V AC with 780 mA LED current

With 230 V AC and 198 V AC input, the PFC always operates in CrCM across the full load range (see **Figure 19**).



(a) 230 V AC, 52 V_{LED}, 1000 mA

(d) 198 V AC, 52 V_{LED}, 1000 mA

(b) 230 V AC, 52 V_{LED}, 880 mA

(e) 198 V AC, 52 V_{LED}, 880 mA

(c) 230 V AC, 52 V_{LED}, 780 mA

(f) 198 V AC, 52 V_{LED}, 780 mA

Figure 19 Steady-state waveform at 230 V AC (a, b, c) and 198 V AC (d, e, f)

The PFC operating frequency at mains peak with 20 V and 52 V LED load is measured and presented in **Table 2** and **Table 3**, respectively.

Table 2 PFC frequency at mains peak with 20 V LED load

PFC frequency at mains peak with 20 V LED	264 V AC	230 V AC	198 V AC
1000 mA	42.9 kHz	78 kHz	83 kHz
880 mA	17 kHz (DCM)	84 kHz	91 kHz
780 mA	**16 kHz** (DCM)	90 kHz	98 kHz

Table 3 PFC frequency at mains peak with 52 V LED load

PFC frequency at mains peak with 52 V LED	264 V AC	230 V AC	198 V AC
1000 mA	**27 kHz**	43 kHz	48 kHz
880 mA	29 kHz	49 kHz	53 kHz
780 mA	32 kHz	53 kHz	58 kHz

The LCC operating frequencies measured at different power settings are listed in **Table 4**.

Table 4 LCC operating frequency at different LED voltage and current settings

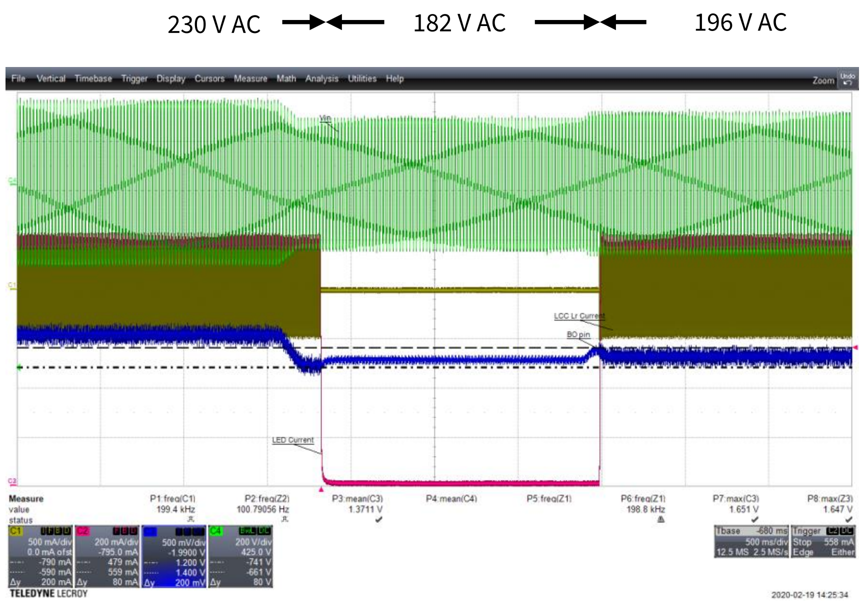
LCC frequency	1000 mA	880 mA	780 mA
52 V_{LED}	171 kHz	228 kHz	244 kHz
20 V_{LED}	194 kHz	256 kHz	265 kHz

3.4 Protections

This section presents the results of brown-out protection and OVP.

3.4.1 Brown-out protection

Figure 20 shows that the driver triggers brown-out protection when the input voltage drops to 182 V AC and the driver recovers operation at 196 V AC.

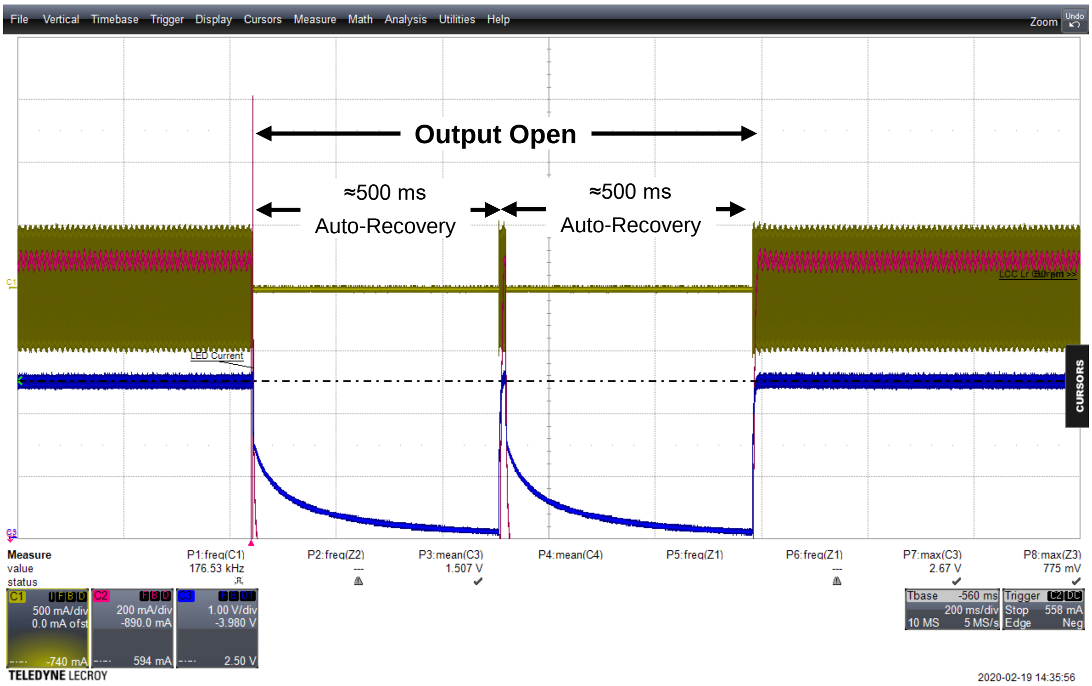


CH1: Resonant inductor current in LCC, CH2: LED current, CH3: Brown-out pin voltage, CH4: Input voltage

Figure 20 Brown-out protection

3.4.2 Output OVP

Figure 21 shows the output OVP when the 52 V LED is disconnected and reconnected. The auto-recovery time is around 500 ms after OVP pin voltage hits 2.5 V.



CH1: Resonant inductor current in LCC, CH2: LED current, CH3: OVP pin voltage

Figure 21 Output OVP

3.5 LED current spread analysis

To reduce the cost of the non-dimmable driver design, open-loop control is one solution that omits the expensive optocoupler used in closed-loop control. However, the LED current spread should be well constrained for a consistent light flux.

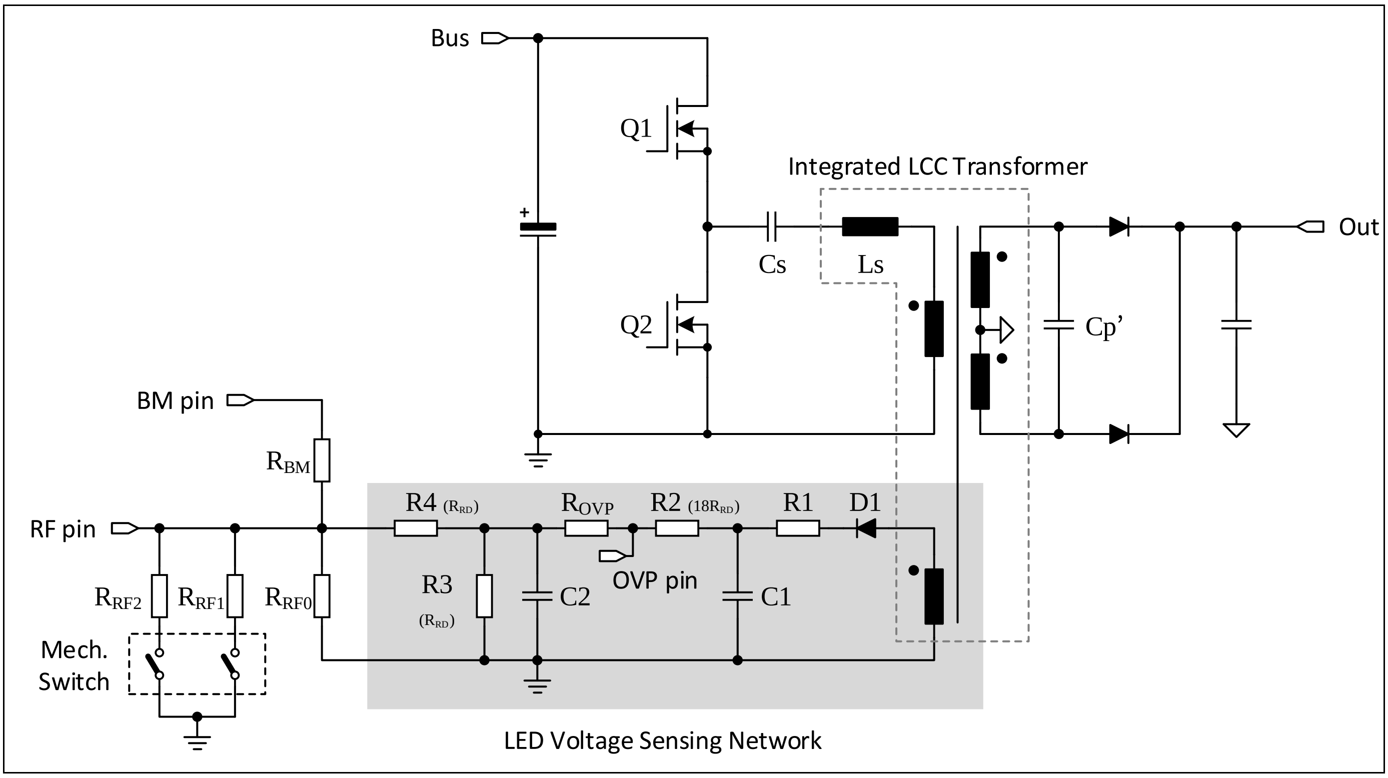


Figure 22 LED current feed-forward compensation from a LED voltage sensing network

If the operating frequency is set only by the resistors R_{BM} and R_{RFx} (see **Figure 22**), the output current will be dependent on the LED voltage. The dashed curve in **Figure 23** shows that lower LED voltage results in a higher LED current, and the influence of varied LED voltage easily deviates the current beyond 10 percent specified tolerance, even without considering the component spread. To limit the LED current dependency on the LED voltage range in the open-loop design, a feed-forward compensation on LED current is implemented by a LED voltage sensing network (see **Figure 22**). Here, an auxiliary winding must be tightly coupled to the secondary windings so as to obtain the accurate LED voltage information. In the integrated LCC transformer of this design, a two-segmented bobbin is utilized for sufficient leakage inductance. The auxiliary winding with a triple isolated wire is wound in the bobbin segment containing two secondary windings and ends back in the segment with the primary winding. In **Figure 22**, D1, R1 and C1 form a network to rectify the AC voltage and damp possible oscillation from parasitic inductance and capacitance. Three subsequent resistors, R2, R3 and R4, tune the frequency sensitivity to the measured LED voltage. Here, R2 is 18 times R3 and R4, which is calculated from the LED maximum voltage and the choice of turns ratio between the secondary winding and the auxiliary winding. R_{OVP} value is much smaller than R2 and R3, which is just slightly tuned for the correct OVP detection.

Simulation has been carried out to investigate the sensitivity of LED current to the LED voltage, in terms of R_{RD} value. Here, R2 = R3 = R_{RD}. To reach the specified LED current, the set frequency (f_{set}) formed only by R_{BM} and R_{RFx} is settled at 160 kHz, 195 kHz and 225 kHz, which can be switched by a mechanical switch. **Figure 23** and **Figure 24** plot the simulated sensitivity at different set frequencies in relation to the R_{RD} value. Conclusions from these simulations are:

1. The LED sensing network is able to effectively reduce the sensitivity of LED voltage on LED current.
2. **R_{RD} = 11 kΩ** is the best choice to flatten the LED current sensitivity over the current settings. The best R_{RD} value can be different only if single current setting is used in the application.

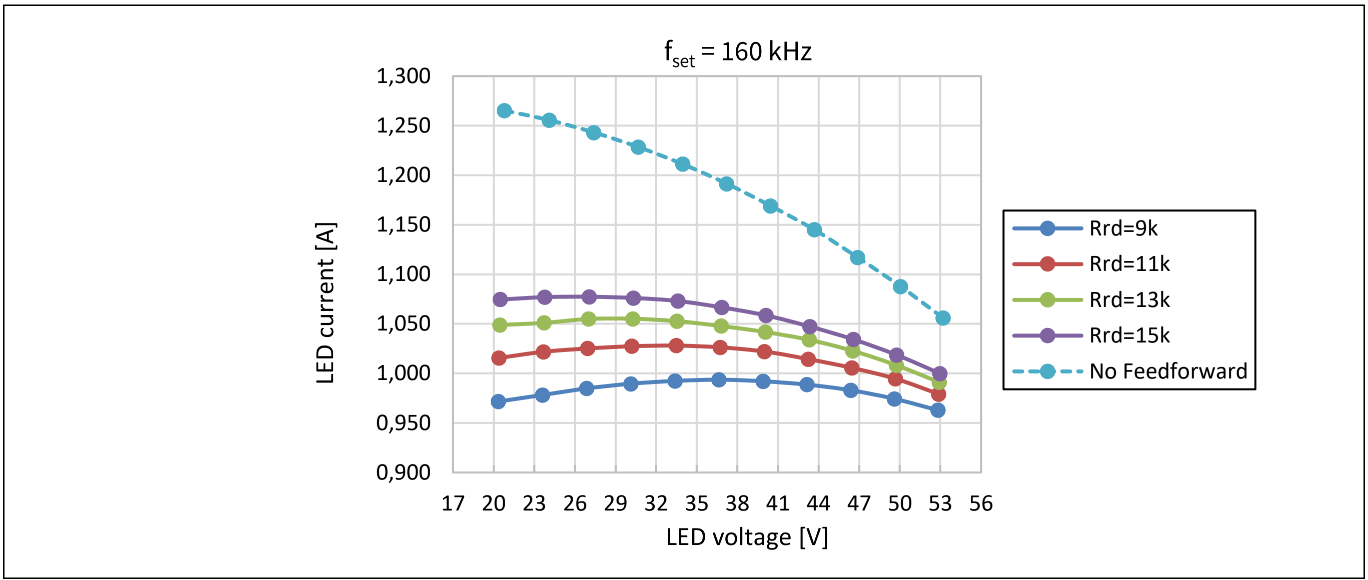


Figure 23 LED current sensitivity simulation in relation to R_{RD} value - f_{set} = 160 kHz

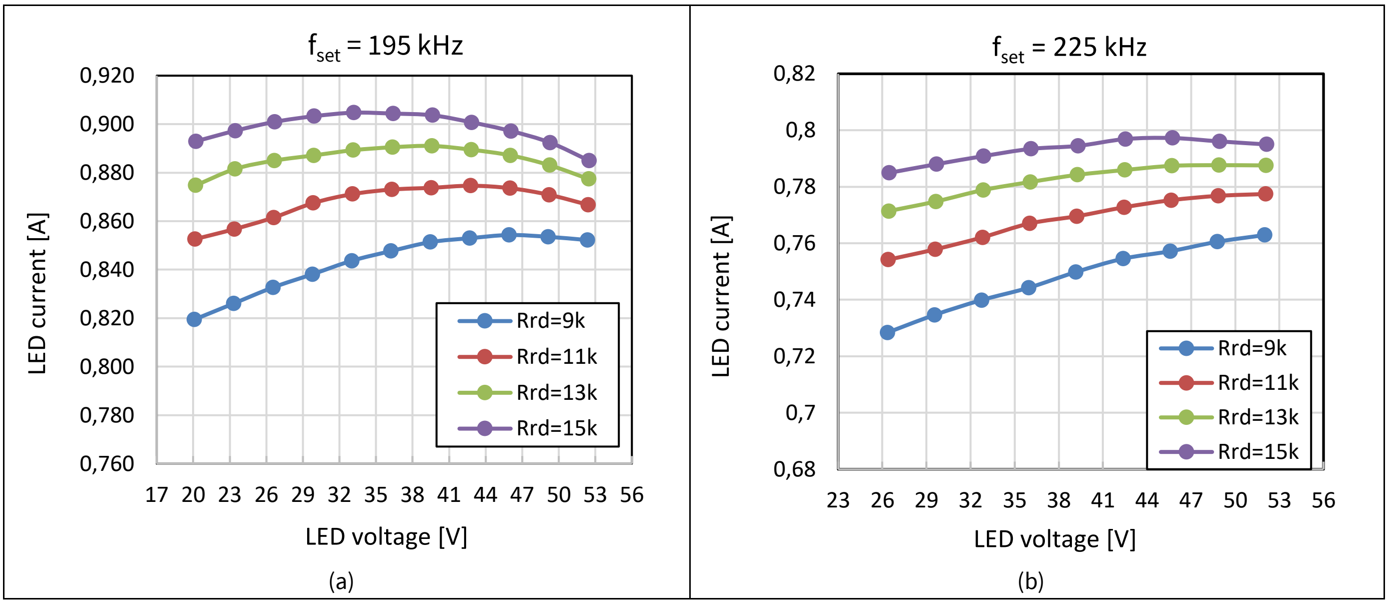


Figure 24 LED current sensitivity simulation in relation to R_{RD} value (a) f_{set} = 195 kHz and (b) f_{set} = 225 kHz

Figure 25 shows the validity of the simulations above.

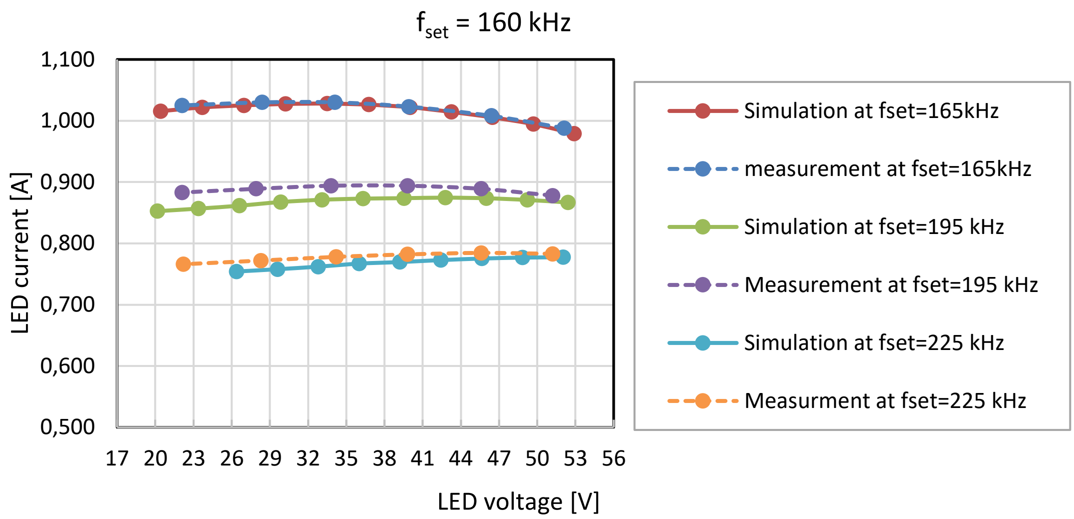


Figure 25 Measurement and simulation comparison

Based on the verified simulation model, the LED current spread has been analyzed based on key component tolerances listed in **Table 5**. The assumption made here is that all component tolerances follow a normal distribution pattern.

Table 5 Component tolerances considered in Monte Carlo analysis for LED current spread

Component	Tolerances	Specified standard deviation	Remarks
Series resonant capacitor (Cs)	±5 percent	3 σ	- Film capacitor
Series resonant inductance (Ls)	±5 percent, ±7 percent, ±10 percent	3 σ	- 5 percent, a standalone inductor - 10 percent, using leakage inductance of a transformer as the resonance inductor
Parallel resonant capacitor (Cp’)	±5 percent	3 σ	- Film capacitor
Resistors	±1 percent	3 σ	- SMD resistor
Frequency as functions of RF pin current	±5 percent	4 σ	- For frequency of less than 210 kHz
	±7 percent	4 σ	For frequency of less than 270 kHz and IC temperature greater than -20°C
Bus voltage	±2 percent	3 σ	- Considering the resistive divider and IC tolerances

In the following analysis, the leakage inductances of the transformer are catergorized into three groups: ±5 percent, ±7 percent and ±10 percent ±5 percent represents a typical inductance tolerance when a discrete inductor is used as the resonance inductor, while ±10 percent represents the typical tolerance where an integrated LCC transformer is implemented. When special care is taken in an integrated transformer design (for example, the windings take a integer number of layers which avoids the leakage inductance variance due to the winding movement in the half-full layer), the leakage inductance can be controlled more tightly than ±10 percent, therefore, ±7 percent is also considered here. The leakage inductance of 50 integrated transformer samples haven’t been tested. Their average inductance, maximum and minimum values and 3-sigma spread have been measured and calculated. **Table 6** presents the statistics of these 50 integrated transformers, where the 3-sigma tolerance of the leakage inductance is 2.84 percent and 1.91 percent for two secondary windings. These transformers are from one product lot. We assume that this value is 7 percent when the lot number increases.

Table 6 Statistics of the leakage inductance of 50 integrated LCC transformer samples

Parameters	Secondary winding 1	Secondary winding 2
Average leakage inductance*	443.8 µH	435 µH
Maximum inductance	453.9 µH	443.3 µH
Minimum inductance	429.2 µH	427.3 µH
Standard deviation	4.2 µH	2.8 µH
3-sigma tolerance**	2.84 percent	1.91 percent

* Measured from primary with one secondary winding shorted and the other one open

** Calculated by 3x standard deviation/average value * 100 percent

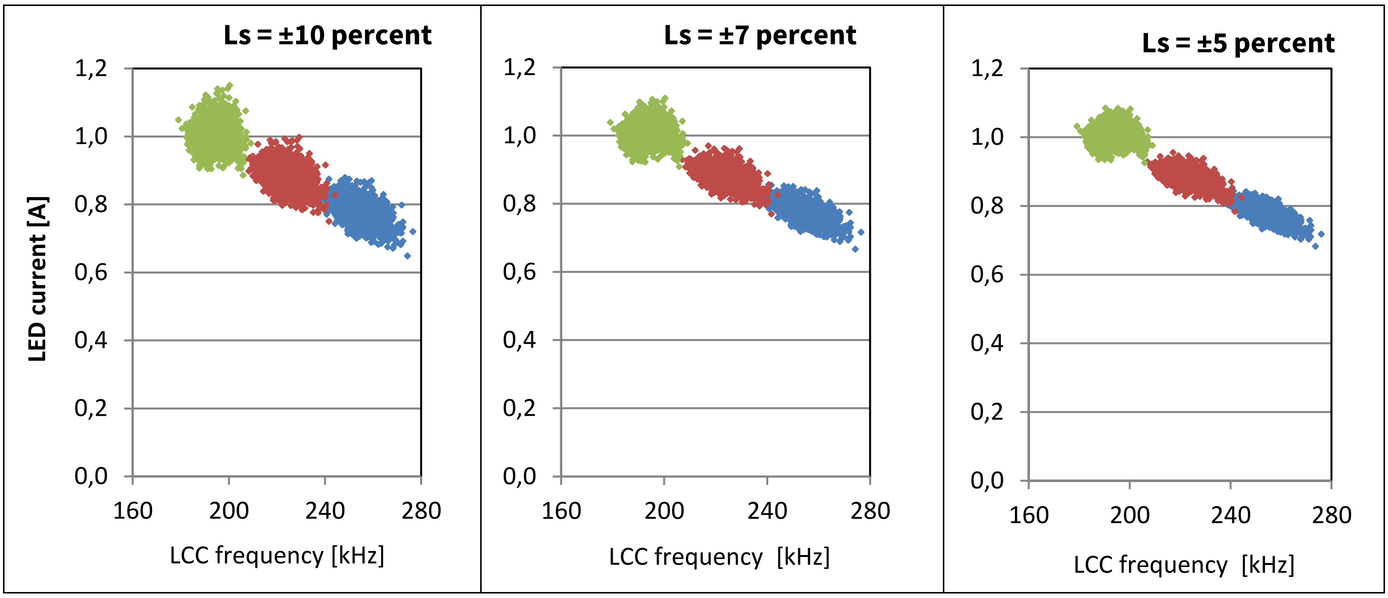
To minimize the LED current spread over the frequency spread caused by the controller IC, the LCC resonance tank must be designed in a special way before the tolerance analysis. The general principle is to make the current gain curve (as a function of frequency) as flat as possible. Here, since this is a non-dimmable design, we do not need to think about the maximum frequency that IC can support at the dimming case.

The selected LCC resonance tank parameters are shown below:

Table 7 LCC resonance tank parameters

LCC resonance tank parameters	Values
Series resonant capacitor (Cs)	47 nF
Series resonant inductance (Ls)	440 uH
Parallel resonant capacitor (Cp') at the secondary side	1.5 nF

In the Monte Carlo simulation, 1600 runs have been done for each current setting and each Ls tolerance group to explore the entired defined tolerance range. The LED current points are plotted in **Figure 26** in terms of the actual LCC frequency and in three different output current settings and full LED voltage range, where the series resonant current tolerances are defined to be ±10 percent, ±7 percent and ±5 percent with 3 σ deviation. In **Figure 26**, the actual LCC frequency spread can be also found. For 1000 mA setting, the LCC frequency is mostly below 210 kHz.



Green: 1000 mA setting, **red**: 880 mA setting, **blue**: 780 mA setting

Figure 26 LED current points in 1600 Monte Carlo simulation runs in specified component tolerance range in Table 5

The LED current spread with different series inductance tolerance groups and three current settings are analysed and shown in **Table 8**. These results show that when Ls = ±7 percent, the LED current spread is successfully controlled within ±10 percent defined in the specification. Note that ±10 percent is normally the typical tolerance of the leakage inductance of a wire-wound transformer, while ±5 percent is a typical inductance of a discrete inductor.

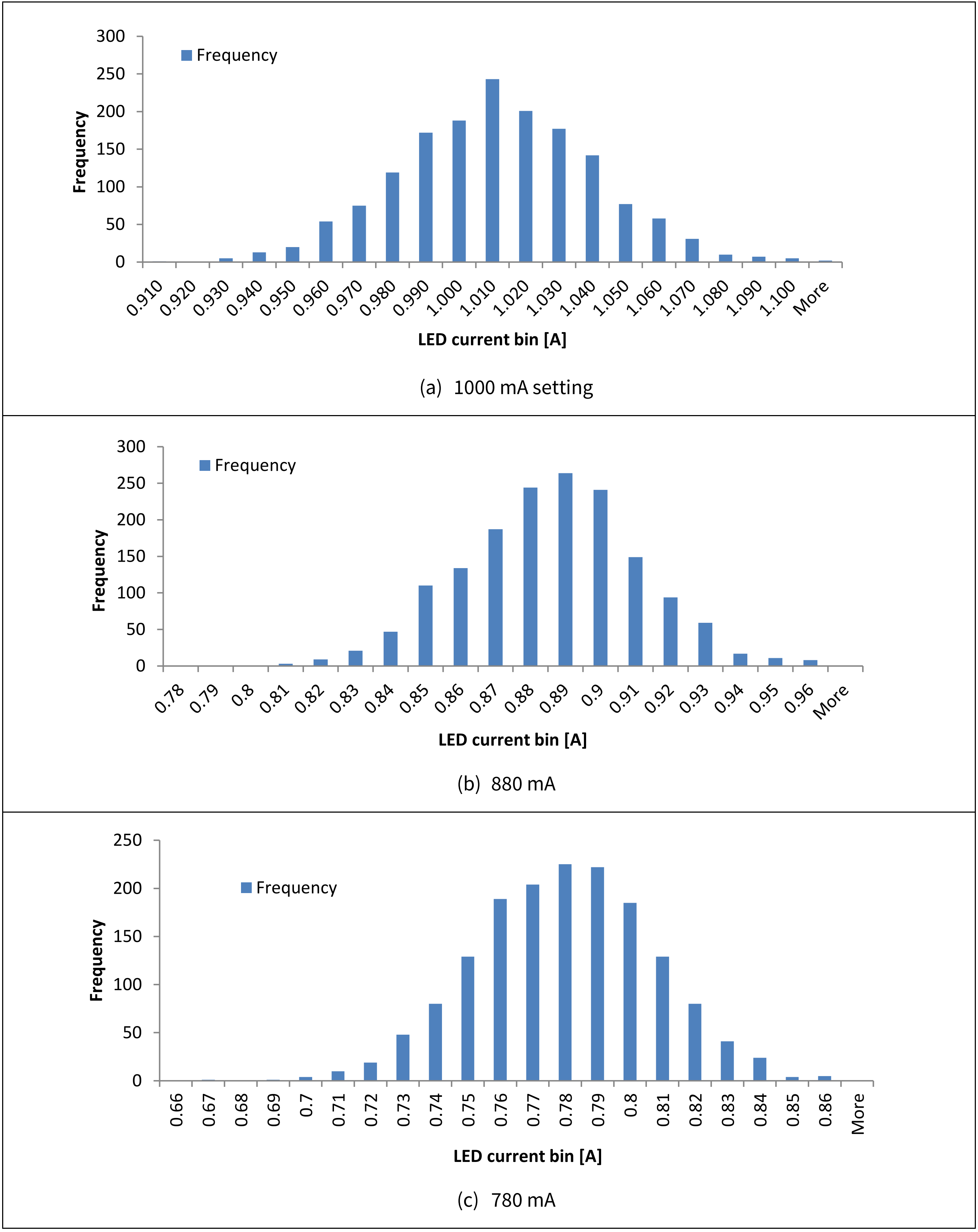
Table 8 LED current spread analysis at different current settings and series inductance tolerance groups

Current settings	Ls = ±10 percent	Ls = ±7 percent	Ls = ±5 percent
1000 mA setting*	±11.2 percent	±8.7 percent	±7.3 percent
880 mA setting	±11.8 percent	±9.4 percent	±7.9 percent
780 mA setting**	±13 percent	±9.96 percent	±9.2 percent

* IC frequency spread here is ±5 percent because the switching frequencies are below 210 kHz

** In this setting, the specified LED voltage is down to 26 V

Figure 27 shows the simulated LED current distribution at three current settings, where all component tolerances listed in **Table 5** have been considered in the Monte Carlo simulation.



(a) 1000 mA setting

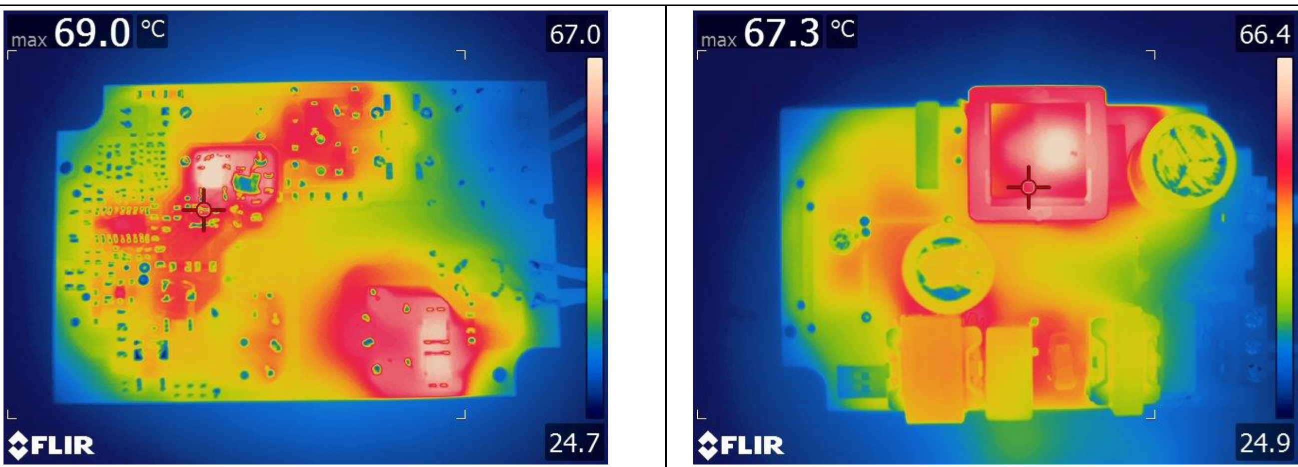
(b) 880 mA

(c) 780 mA

Figure 27 Simulated LED current distribution with Ls = ±7 percent and at (a) 1000 mA, (b) 880 mA and (c) 780 mA current settings

4 Thermal performance

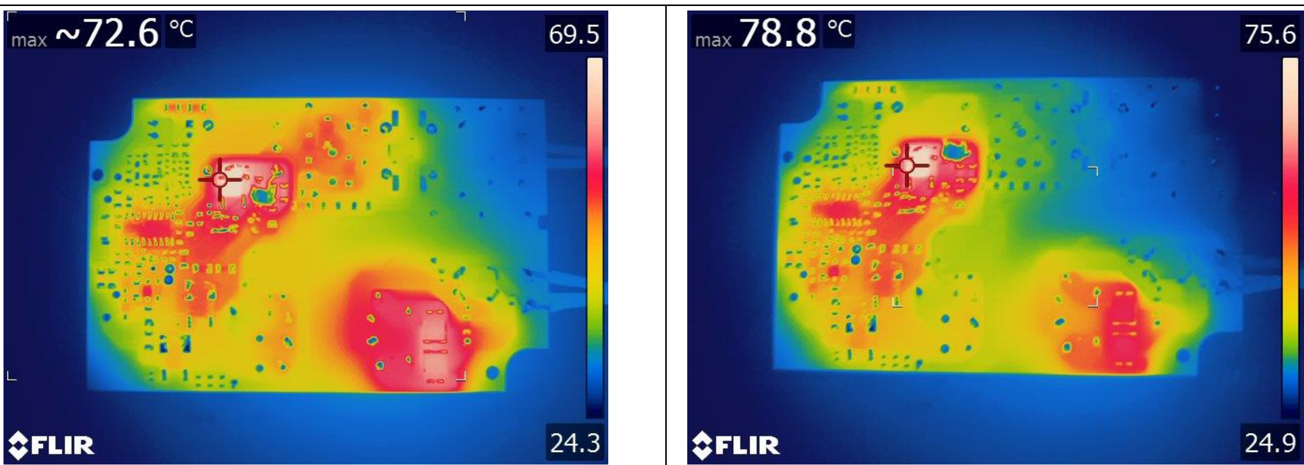
Figure 28 shows the infrared picture of the board at nominal input and full load, namely 230 V AC input and 100 mA/52 V LED, with 23°C room temperature and free air condition.



(a) SMD component side | (b) Through-hole component side

Figure 28 Thermal at nominal condition: 230 V AC, 52 V_{LED} and 1000 mA (23°C room temperature and free air)

Figure 29(a) shows the thermal situation when the input is maximum (264 V AC) with full load. The boost MOSFET reaches 72.6°C. Figure 29(b) shows the temperature profile when the input is 264 V AC. Here, the load is low with 880 mA, 23 V_{LED}, but the PFC operates in DCM, similar to Figure 17(c).

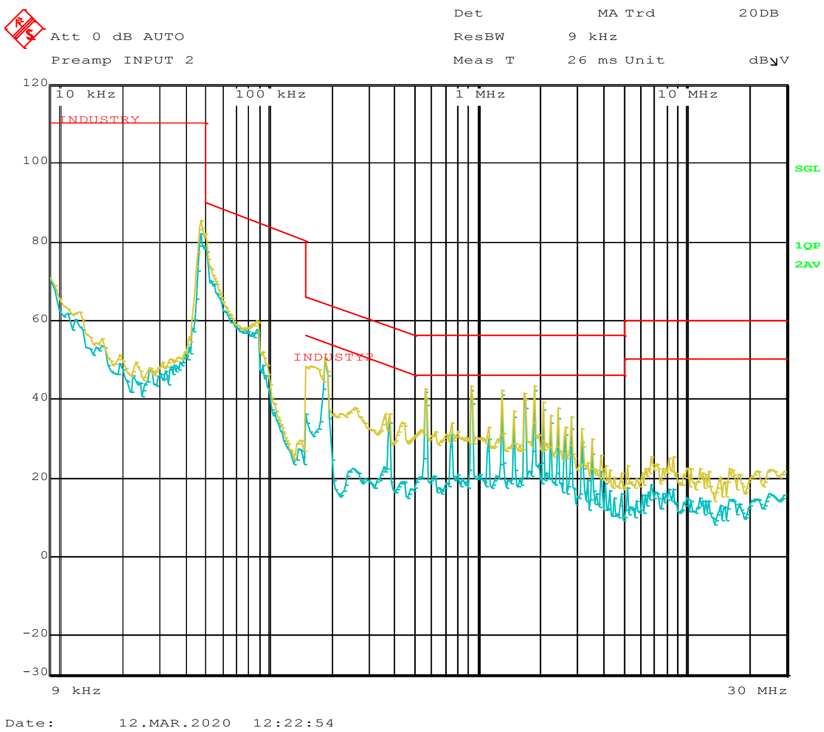


(a) 264 V AC, 52 V_{LED}, 1000 mA | (b) 264 V, 23 V_{LED}, 880 mA

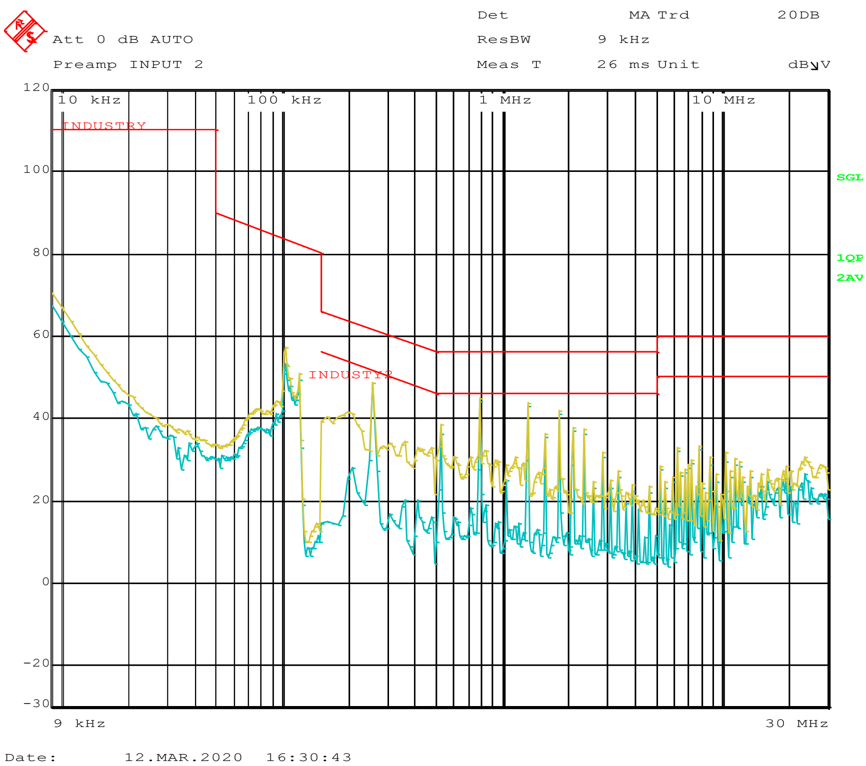
Figure 29 Worst thermal case (23°C room temperature and free air)

5 EMI

The figures below show the conducted EMI at 1 A, 52 V_{LED} and 0.78 A, 26 V_{LED}. In the latter case, the PFC runs in DCM.



Full load – 230 V AC, 52 V_{LED}, 1 A



Minimum load – 230 V AC, 26 V_{LED}, 780 mA

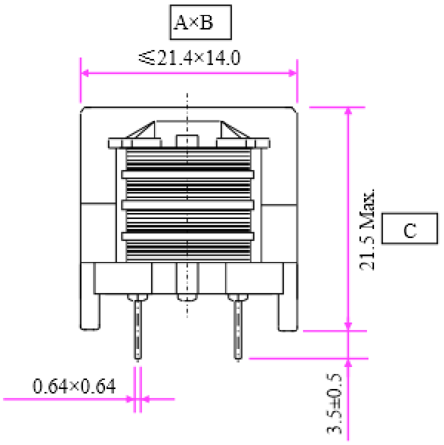
6 Magnetic component datasheets

The datasheets of the common-mode EMI filter, boost inductor and LCC transformer are given below.

Common mode filter (L10):

ICT INTELLIGENT COMPONENTS TECHNOLOGY ZHUHAI LTD. (CHINA)	CUSTOMER :	INFINEON	Page 2 of 2
	DESCRIPTION:	EF20/10/06 X'Fmr	
Product Specification	CUSTOMER P/N :	(NP2019-13911)	CUSTOMER Rev.:
	ICT NPR No. :	NP2019-13911	ICT Rev.: A

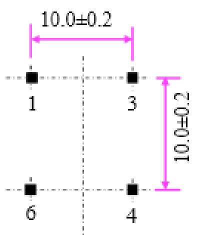
MECHANICAL (UNIT: mm)



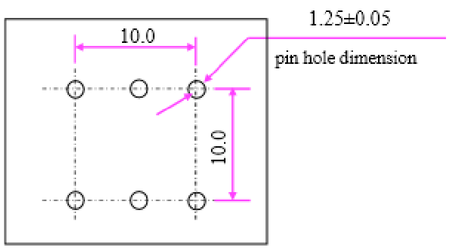
Marking

ICT PRC ..
NP13911

..Date code(week/year)



PIN VIEW

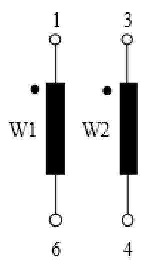


pin hole gauge drawing

ELECTRICAL SPECIFICATION @25℃

TURNS RATIO	: W1:W2=130.5Ts:130.5Ts
L(1-6)(3-4)	: 39mH+50%/-30% @10kHz, 50mV
L_L(1-6)	: 0.5~1.1mH @10kHz, 50mV, shorted W2
DCR(1-6)(3-4)	: 2.1Ω Max.
HI-POT	: 1500Vrms(W1 to W2) @50Hz, for 2Sec.

SCHEMATICS



MATERIALS:

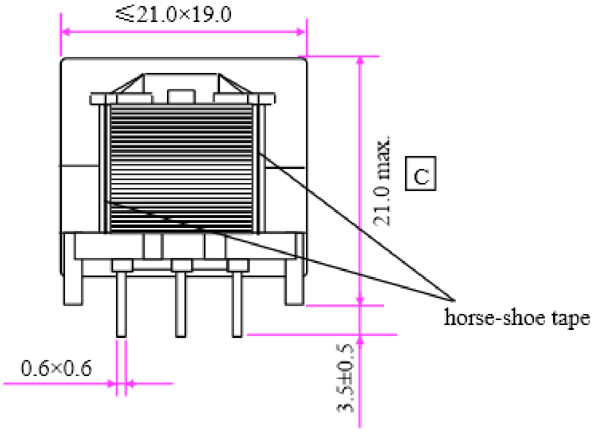
Bobbin	: EF20, Vertical, 4Sec, 4Pins, PET(FR530) or A3X2G7 or equal
CORE	: EF20/10/6, TS5 or KL5 or R5K or HS502 or equal
WIRE	: (W1,W2) Φ0.25mm, UEW , 155℃
GLUE	: F121A/B or F330A/B or LO-200A/B

Rev.	Change history
A	

Boost inductor (L7):

ICT INTELLIGENT COMPONENTS TECHNOLOGY ZHUHAI LTD (CHINA)	CUSTOMER :	INFINEON	Page 2 of 2
	DESCRIPTION:	EF20/09/11 X'Fmr	
Product Specification	CUSTOMER P/N :	(NP2019-13912)	CUSTOMER Rev.:
	ICT NPR No. :	NP2019-13912	ICT Rev.: A

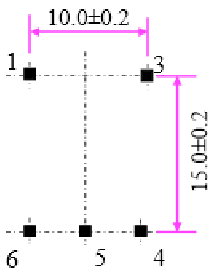
MECHANICAL (UNIT: mm)



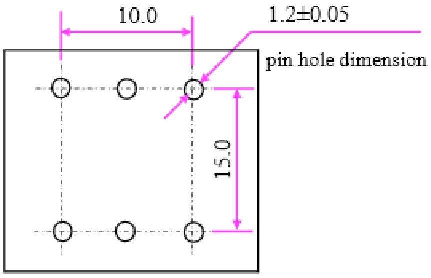
Marking

ICT PRC ..
NP13912

.. Date code

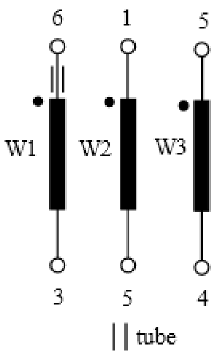


PIN VIEW



pin hole gauge drawing

SCHEMATICS



ELECTRICAL SPECIFICATION @25℃

TURNS RATIO	: W1:W2:W3=121.5Ts:18.5Ts:5Ts
L(6-3)	: 1.8mH±5% @10kHz, 50mV
HI-POT	: 1500Vrms(Wdgs to Core) @50Hz, for 1Sec.
	: 500Vrms(W1 to W2,W3) @50Hz, for 1Sec.

MATERIALS:

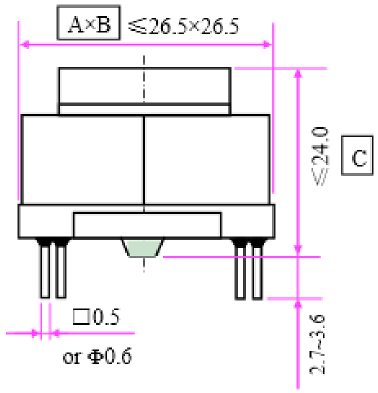
BOBBIN	: EF20/11, Vertical, 1 Section, 5 Pins, FR530 or A3X2G7 or equal
CORE	: EF20/9/11, TP4A or HC44 or PG242 or KP44 or DMR44, Gap≈2×0.40mm
WIRE	: (W1)10×Φ0.10mm, UEW , 155℃
	: (W2,W3)Φ0.23mm or Φ0.224mm, UEW +NY,155°C
TAPE	: 11.4mm wide, CT280 or #1350F or equal
TUBE	: Teflon tube, AWG#26
GLUE	: F121A/B or F330A/B or LO-200A/B or equal
	: SP2316

Rev.	Change history
A	

LCC transformer (T300A):

ICT 珠海科德电子有限公司 INTELLIGENT COMPONENTS TECHNOLOGY ZHUHAI LTD. (CHINA)	CUSTOMER :	INFINEON	Page 2 of 2
	DESCRIPTION:	EF25/13/11 X'Fmr	
Product Specification	CUSTOMER P/N :	(NP2019-13822)	CUSTOMER Rev.:
	ICT NPR No. :	NP2019-13822	ICT Rev.: A3

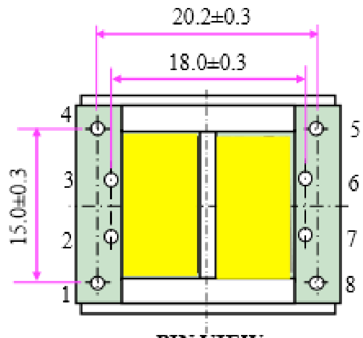
MECHANICAL (UNIT: mm)



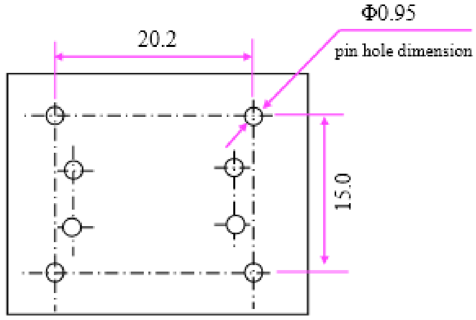
Marking

ICT PRC ..
● NP13822 A3

.. Date code



PIN VIEW

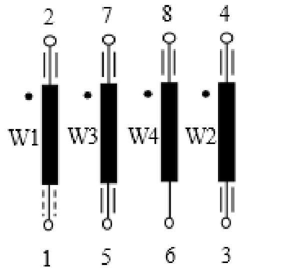


pin hole gauge drawing

ELECTRICAL SPECIFICATION @25℃

TURNS RATIO	: W1:W3:W4:W2=84Ts:24Ts:24Ts:12Ts
L(2-1)	: 13.5～29.0mH @100KHz,50mV
L_{L1}(2-1)	: 433uH±10% @100KHz,50mV,shorted W3
L_{L2}(2-1)	: 433uH±10% @100KHz,50mV,shorted W4
HI-POT	: 4500Vrms(W1,W2 to W3,W4) @50Hz, for 2Sec.
	: 1000Vrms(Wdgs to Core) @50Hz, for 2Sec.

SCHEMATICS



|| :tube
¦¦ :tube (optional)

MATERIALS:

COVER	: EF25/13/11, A3X2G7 or FR530 or equal
BOBBIN	: EF25/13/11, Horizontal, 2sections, A3X2G7 or FR530 or equal
CORE	: EF25/13/11, TP4A or DMR44 or KP44 or HC44 or PG242 or equal
WIRE	: (W1)25×Φ0.071mm, UEW, 155°C
	: (W3,W4)40×Φ0.071mm, UEW, 155°C,
	: (W2)Φ0.20mm, Triple insulation wire, TEX-E or TIW-M or TRW-B or TIW-B or E&B-XXXB-1 or equal
TAPE	: 7.0mm wide, *1350F or CT280 or equal
TUBE	: Teflon tube, AWG#24 & AWG#22
GLUE	: F305A/B or F121A/B or equal

Rev.	Change history
A3	

7 Electronics BOM

The BOM is shown below.

No.	Quantity	Designator	Description
1	1	C1	Capacitor 2.2 nF/250 V/CAPRR1000W60L900T700H1200B/20 percent
2	1	C2	Capacitor 100 nF/25 V/0603/X7R/5 percent
3	1	C3	Capacitor 330 nF/630 V/CAPRR1500W80L1800T800H1400B/20 percent
4	1	C10	Capacitor 220 nF/305 V/CAPRR1500W80L1800T700H1250B/10 percent
5	1	C12	Capacitor 2.2 nF/630 V/CAPC3216X125N/X7R/10 percent
6	1	C200	Capacitor 330 pF/630 V/1206/C0G/5 percent
7	1	C201	Capacitor 22 µF/450 V/CAPPRD750W80D1625H2700B-B/20 percent
8	1	C300	Capacitor 1 µF/25 V/1206 (3216)/10 percent
9	1	C302	Capacitor 10 µF/63 V/CAPPRD200W50D500H1200B/20 percent
10	1	C303	Capacitor 180 pF/630 V/1206/C0G/5 percent
11	1	C304	Capacitor 100 nF/50 V/0805/X7R/10 percent
12	1	C307	Capacitor 47 nF/1 kV/CAPRR1500W80L1800T700H1250B/10 percent
13	1	C308	Capacitor 470 nF/50 V/603/X7R/10 percent
14	3	C309, C316, C318	Capacitor 1 nF/25 V/0603/C0G/5 percent
15	1	C311	Capacitor 3.3 nF/50 V/0603/C0G/5 percent
16	1	C312	Capacitor 100 pF/50 V/0805 (2012)/C0G/5 percent
17	1	C317	Capacitor 33 nF/25 V/0603/X7R/5 percent
18	1	C319	Capacitor 100 pF/50 V/0603/C0G/2 percent
19	1	C400	Capacitor 1.5 nF/1.6 kV/CAPRR1000W60L1300T500H1100B/5 percent
20	1	C401	Capacitor 330 µF/100 V/CAPPRD750W80D1850H2150B/20 percent
21	1	C500	Capacitor 1 µF/25 V/0805/X7R/10 percent
22	1	CY100	Capacitor 2.2 nF/X1/Y1, 760 V, 500 V/Disc/20 percent
23	2	D10, D11	Diode S1PM/1 kV/1 A/DO-220AA (SMP)/
24	4	D17, D21, D22, D23	Diode S1M/1 kV/1 A/DO-214AC (SMA)/
25	2	D200, D201	Diode ES1J/na, 600 V/1 A/SMA (DO-214AC)/
26	4	D300, D301, D303, D305	Diode 1N4148W/100 V/300 mA/SOD123/
27	2	D400, D401	Diode TSP10H200S/200 V/10 A/TO-277A (SMPC)/
28	1	DZ302	Diode 18 V/SOD123/
29	1	F1	Fuse 3.15 A/300 V/FUSRR508W60L850T400H800B/
30	2	L1, L2	Inductor ferrite bead/7 A/THT/
31	1	L7	Inductor 10082865F/EF20-11/
32	1	L10	Inductor 39 mH/F20-10 -6/
33	1	L400	Inductor 25 µH/SMT/
34	3	Q200, Q201, Q202	Transformer IPN60R600P7S/650 V/PG-SOT223-3/
35	1	R2	Resistor 550 V AC/745 V/Radial
36	3	R12, R13, R14	Resistor 2.2 MEG/200 V/1206/1 percent
37	2	R92, R93	Resistor 33 k/150 V/0805/1 percent

38	3	R104, R105, R106	Resistor 200 k/200 V/1206/1 percent
39	2	R200, R201	Resistor 33 R/200 V/1206/5 percent
40	3	R202, R205, R208	Resistor 1.2 MEG/200 V/1206/1 percent
41	1	R203	Resistor 22 R/150 V/0805/1 percent
42	1	R204	Resistor 220 k/150 V/0805/1 percent
43	2	R209, R323	Resistor 0 R/150 V/0805
44	3	R210, R211, R212	Resistor 2.2 R/150 V/0805/1 percent
45	1	R300	Resistor 1 R/200 V/1206/1 percent
46	1	R301	Resistor 10 R/200 V/1206/1 percent
47	2	R302, R304	Resistor 47 R/150 V/0805/1 percent
48	2	R303, R307	Resistor 51 k/75 V/0603/1 percent
49	1	R305	Resistor 51 k/150 V/0805/1 percent
50	1	R306	Resistor 510 R/150 V/0805/1 percent
51	1	R308	Resistor 470 R/75 V/0603/1 percent
52	3	R310, R311, R312	Resistor 1 R/150 V/0805/1 percent
53	1	R313	Resistor 39 k/75 V/0603/1 percent
54	1	R315	Resistor 0 R/200 V/1206/
55	1	R316	Resistor 22 k/75 V/0603/1 percent
56	2	R317, R339	Resistor 100 k/0603/1 percent
57	1	R320	Resistor 1 k/150 V/0805/1 percent
58	2	R324, R337	Resistor 11 k/75 V/0603/1 percent
59	1	R325	Resistor 4.3 k/75 V/0603/1 percent
60	1	R326	Resistor 200 k/75 V/0603/1 percent
61	1	R333	Resistor 510 k/75 V/0603/1 percent
62	2	R334, R336	Resistor 0 R/75 V/0603/1 percent
63	1	R335	Resistor 6.2 k/75 V/0603/1 percent
64	1	R401	Resistor 100 k/200 V/1206/1 percent
65	2	R402, R403	Resistor 100 k/150 V/0805/1 percent
66	1	S1	Switch 2-pos/DIP-4
67	1	T300	Transformer NP13822/THT
68	1	U300	IC ICL5102/PG-DSO-16
69	1	X10	Connector 1888690/CON-TER-THT-MKDSN 2,5_3-5,08
70	1	X101	Connector 1729128/CON-TER-THT-MKDSN 1,5_2-5,08
71	0	R10, R11	Resistor NA/500 V/2512/0 R
72	0	R206	Resistor NA/75 V/0603/1 percent
73	0	R309, R338	Resistor NA/75 V/0603/1 percent
74	0	R319	Resistor NA/150 V/0805/1 percent
75	0	X1, X301	Con JL-1000-25-T/JP-THT-JL-1000-25-T
76	0	X2, X3	Con JP-THT-L-17.5 mm/JP-THT-1.00_2.20_17.5_0.80-2P
77	0	X11, X12	Con JL-250-25-T/JP-THT-JL-250-25-T

Revision history

Document version	Date of release	Description of changes
V 1.0	14-07-2020	First release

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